

November 2, 2018

RE: CERTIFICATION LETTER

Project/Job # 604008

Project Address: Guzinski Residence

8917 Wheeler Dr Orland Park, IL 60462

AHJ Orland Park village SC Office Chicago-Temp

Design Criteria:

- Applicable Codes = 2015 IEBC/IBC, 2015 IRC, ASCE 7-10, and 2015 NDS
- Risk Category = II
- Wind Speed = 115 mph, Exposure Category C, Partially/Fully Enclosed Method
- Ground Snow Load = 30 psf
- MP1: Roof DL = 8.5 psf, Roof LL/SL = 30 psf
- MP3: Roof DL = 7.5 psf, Roof LL/SL = 30 psf
- MP5: Roof DL = 7.5 psf, Roof LL/SL = 30 psf

Note: Per IBC 1613.1; Seismic check is not required because Ss = 0.18493 < 0.4g and Seismic Design Category (SDC) = B < D

To Whom It May Concern,

A jobsite survey of the existing framing system of the address indicated above was performed by a site survey team from Tesla. Structural evaluation was based on site observations and the design criteria listed above.

Based on this evaluation, I certify that the alteration to the existing structure by installation of the PV system, with upgrades specified in the plans, meets the requirements of the applicable existing building and/or new building provisions adopted/referenced above.

Additionally, I certify that the PV module assembly including all standoffs supporting it have been reviewed to be in accordance with the manufacturer's specifications and to meet and/or exceed all requirements set forth by the referenced codes for loading.

The PV assembly hardware specifications are contained in the plans/docs submitted for approval.

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HARDWARE DESIGN AND STRUCTURAL ANALYSIS RESULTS SUMMARY TABLES

Landscape	Hardware - Landscape Modules' Standoff Specifications						
Hardware	X-X Spacing	X-X Cantilever	Y-Y Spacing	Y-Y Cantilever	Configuration	Uplift DCR	
MP1	48"	24"	41"	NA	Staggered	31.6%	
MP3	48"	24"	41"	NA	Staggered	28.0%	
MP5	48"	24"	41"	NA	Staggered	28.0%	

Portrait	Hardware - Portrait Modules' Standoff Specifications						
Hardware	X-X Spacing	X-X Cantilever	Y-Y Spacing	Y-Y Cantilever	Configuration	Uplift DCR	
MP1	48"	20"	62"	NA	Staggered	47.8%	
MP3	48"	20"	62"	NA	Staggered	42.3%	
MP5	48"	20"	62"	NA	Staggered	42.3%	

Mounting Plans	Roof Pitch	Qualification Results
Mounting Plane	(Degrees)	Member Evaluation Results
MP1	26°	Member Analysis OK
MP3	26°	Member Analysis OK
MP5	26°	Member Analysis OK



STRUCTURE ANALYSIS - LOADING SUMMARY AND MEMBER CHECK - MP1

Member Loading Summary								
Roof Pitch	Roof Pitch 6/12 Initial Pitch Adjust Non-PV Areas PV Areas							
Roof Dead Load	DL	8.5 psf	x 1.11	9.5 psf	9.5 psf			
PV Dead Load	PV-DL	3.0 psf	x 1.11		3.3 psf			
Roof Live Load	RLL	20.0 psf	x 0.90	18.0 psf				
Live/Snow Load	LL/SL ^{1,2}	30.0 psf	x1 lx1	30.0 psf	30.0 psf			
Total Load (Governing LC)	TL			39.5 psf	42.8 psf			

Notes: 1. ps = Cs*pf; Cs -roof, Cs -pv per ASCE 7 [Figure 7-2] 2. pf = $0.7 (C_e) (C_t) (I_s) p_g$; C_e =0.9, C_t =1.1, I_s =1.0

Member Analysis Results Summary						
Governing Analysis Max Moment @ Location Capacity DCR Result						
(-) Bending Stress (psi) -659.5 17.0 ft -649.9 101% Pass						

ZEP HARDWARE DESIGN CALCULATIONS - MP1

Mounting Plane Information						
Roofing Material	Comp Roof					
Roof Slope	26°					
Framing Type / Direction	Y-Y Rafters					
PV System Type	SolarCity SleekMount™					
Zep System Type	ZS Comp					
Standoff (Attachment Hardware)	Comp Mount SRV					
Spanning Vents	No					

Wind Design Criteria						
Design Code	IBC 2015	ASCE 7-10				
Wind Design Method		Partially/Fully Enclosed Method				
Ultimate Wind Speed	V-UIt	115 mph	Fig. 1609A			
Exposure Category		C	Section 26.7			
Roof Style		Gable Roof	Fig. 30.4-2A/B/C-5A/B			
Mean Roof Height	h	25 ft	Section 26.2			

Wind Pressure Calculation Coefficients					
Wind Pressure Exposure	K _z	0.95	Table 30.3-1		
Topographic Factor	K _{zt}	1.00	Section 26.8		
Wind Directionality Factor	K _d	0.85	Section 26.6-1		
Importance Factor	1	NA			
Velocity Pressure	q _h	qh = 0.00256 (Kz) (Kzt) (Kd) (V^2) 27.2 psf	Equation 30.3-1		

		Wind Pressure	
Ext. Pressure Coefficient (Up)	GCp (Up)	-0.88	Fig. 30.4-2A/B/C-5A/B
Ext. Pressure Coefficient (Down)	GCp (Down)	0.45	Fig. 30.4-2A/B/C-5A/B
Design Wind Pressure	р	p = qh (GCp)	Equation 30.4-1
Wind Pressure Up	p _(up)	-23.8 psf	
Wind Pressure Down	p _(down)	16.0 psf	

ALLOWABLE STANDOFF SPACINGS

		X-Direction	Y-Direction
Max Allowable Standoff Spacing	Landscape	48"	41''
Max Allowable Cantilever	Landscape	24"	NA
Standoff Configuration	Landscape	Staggered	
Max Standoff Tributary Area	Trib	14 sf	
PV Assembly Dead Load	W-PV	3.0 psf	
Net Wind Uplift at Standoff	T-actual	-173 lbs	
Uplift Capacity of Standoff	T-allow	548 lbs	
Standoff Demand/Capacity	DCR	31.6%	

		X-Direction	Y-Direction
Max Allowable Standoff Spacing	Portrait	48"	62"
Max Allowable Cantilever	Portrait	20"	NA
Standoff Configuration	Portrait	Staggered	
Max Standoff Tributary Area	Trib	21 sf	
PV Assembly Dead Load	W-PV	3.0 psf	
Net Wind Uplift at Standoff	T-actual	-262 lbs	
Uplift Capacity of Standoff	T-allow	548 lbs	
Standoff Demand/Capacity	DCR	47.8%	

STRUCTURE ANALYSIS - LOADING SUMMARY AND MEMBER CHECK - MP3

Member Loading Summary							
Roof Pitch 6/12 Initial Pitch Adjust Non-PV Areas PV Areas							
Roof Dead Load	DL	7.5 psf	x 1.11	8.3 psf	8.3 psf		
PV Dead Load	PV-DL	3.0 psf	x 1.11		3.3 psf		
Roof Live Load	RLL	20.0 psf	x 0.90	18.0 psf			
Live/Snow Load	LL/SL ^{1,2}	30.0 psf	x1 lx1	30.0 psf	30.0 psf		
Total Load (Governing LC)	TL			38.3 psf	41.7 psf		

Notes: 1. ps = Cs*pf; Cs -roof, Cs -pv per ASCE 7 [Figure 7-2] 2. pf = $0.7 (C_e) (C_t) (I_s) p_g$; C_e =0.9, C_t =1.1, I_s =1.0

Member Analysis Results Summary						
Governing Analysis Max Moment @ Location Capacity DCR Result						
(+) Bending Stress (psi)	1,408.5	8.2 ft	1,461.4	96%	Pass	

ZEP HARDWARE DESIGN CALCULATIONS - MP3

Mounting Plane Information				
Roofing Material	Comp Roof			
Roof Slope	26°			
Framing Type / Direction	Y-Y Rafters			
PV System Type	SolarCity SleekMount™			
Zep System Type	ZS Comp			
Standoff (Attachment Hardware)	Comp Mount SRV			
Spanning Vents	No			

Wind Design Criteria			
Design Code	IBC 2015	ASCE 7-10	
Wind Design Method		Partially/Fully Enclosed Method	
Ultimate Wind Speed	V-Ult	115 mph	Fig. 1609A
Exposure Category		С	Section 26.7
Roof Style		Gable Roof	Fig. 30.4-2A/B/C-5A/B
Mean Roof Height	h	15 ft	Section 26.2

Velocity Pressure	q _h	qh = 0.00256 (Kz) (Kzt) (Kd) (V^2) 24.4 psf	Equation 30.3-1		
Importance Factor	1	NA			
Wind Directionality Factor	K_d	0.85	Section 26.6-1		
Topographic Factor	K _{zt}	1.00	Section 26.8		
Wind Pressure Exposure	K_z	0.85	Table 30.3-1		
Wind Pressure Calculation Coefficients					

		Wind Pressure	
Ext. Pressure Coefficient (Up)	GCp (Up)	-0.88	Fig. 30.4-2A/B/C-5A/B
Ext. Pressure Coefficient (Down)	GCp (Down)	0.45	Fig. 30.4-2A/B/C-5A/B
Design Wind Pressure	р	p = qh (GCp)	Equation 30.4-1
Wind Pressure Up	p _(up)	-21.4 psf	
Wind Pressure Down	p _(down)	16.0 psf	

ALLOWABLE STANDOFF SPACINGS

		X-Direction	Y-Direction
Max Allowable Standoff Spacing	Landscape	48"	41''
Max Allowable Cantilever	Landscape	24"	NA
Standoff Configuration	Landscape	Staggered	
Max Standoff Tributary Area	Trib	14 sf	
PV Assembly Dead Load	W-PV	3.0 psf	
Net Wind Uplift at Standoff	T-actual	-153 lbs	
Uplift Capacity of Standoff	T-allow	548 lbs	
Standoff Demand/Capacity	DCR	28.0%	

		X-Direction	Y-Direction
Max Allowable Standoff Spacing	Portrait	48''	62''
Max Allowable Cantilever	Portrait	20"	NA
Standoff Configuration	Portrait	Staggered	
Max Standoff Tributary Area	Trib	21 sf	
PV Assembly Dead Load	W-PV	3.0 psf	
Net Wind Uplift at Standoff	T-actual	-232 lbs	
Uplift Capacity of Standoff	T-allow	548 lbs	
Standoff Demand/Capacity	DCR	42.3%	

STRUCTURE ANALYSIS - LOADING SUMMARY AND MEMBER CHECK - MP5

Member Loading Summary						
Roof Pitch 6/12 Initial Pitch Adjust Non-PV Areas PV Areas						
Roof Dead Load	DL	7.5 psf	x 1.11	8.3 psf	8.3 psf	
PV Dead Load	PV-DL	3.0 psf	x 1.11		3.3 psf	
Roof Live Load	RLL	20.0 psf	x 0.90	18.0 psf		
Live/Snow Load	LL/SL ^{1,2}	30.0 psf	x1 lx1	30.0 psf	30.0 psf	
Total Load (Governing LC)	TL			38.3 psf	41.7 psf	

Notes: 1. ps = Cs*pf; Cs -roof, Cs -pv per ASCE 7 [Figure 7-2] 2. pf = $0.7 (C_e) (C_t) (I_s) p_g$; C_e =0.9, C_t =1.1, I_s =1.0

Member Analysis Results Summary						
Governing Analysis Max Moment @ Location Capacity DCR Result						
(+) Bending Stress (psi)	1,122.1	7.6 ft	1,461.4	77%	Pass	

ZEP HARDWARE DESIGN CALCULATIONS - MP5

Mounting Plane Information				
Roofing Material	Comp Roof			
Roof Slope	26°			
Framing Type / Direction	Y-Y Rafters			
PV System Type	SolarCity SleekMount™			
Zep System Type	ZS Comp			
Standoff (Attachment Hardware)	Comp Mount SRV			
Spanning Vents	No			

Wind Design Criteria			
Design Code	IBC 2015	ASCE 7-10	
Wind Design Method		Partially/Fully Enclosed Method	
Ultimate Wind Speed	V-Ult	115 mph	Fig. 1609A
Exposure Category		С	Section 26.7
Roof Style		Gable Roof	Fig. 30.4-2A/B/C-5A/B
Mean Roof Height	h	15 ft	Section 26.2

Wind Pressure Calculation Coefficients					
Wind Pressure Exposure	K _z	0.85	Table 30.3-1		
Topographic Factor	K _{zt}	1.00	Section 26.8		
Wind Directionality Factor	K _d	0.85	Section 26.6-1		
Importance Factor	1	NA			
Velocity Pressure	q _h	qh = 0.00256 (Kz) (Kzt) (Kd) (V^2) 24.4 psf	Equation 30.3-1		

		Wind Pressure	
Ext. Pressure Coefficient (Up)	GCp (Up)	-0.88	Fig. 30.4-2A/B/C-5A/B
Ext. Pressure Coefficient (Down)	GCp (Down)	0.45	Fig. 30.4-2A/B/C-5A/B
Design Wind Pressure	р	p = qh (GCp)	Equation 30.4-1
Wind Pressure Up	p _(up)	-21.4 psf	
Wind Pressure Down	p _(down)	16.0 psf	

ALLOWABLE STANDOFF SPACINGS

		X-Direction	Y-Direction
Max Allowable Standoff Spacing	Landscape	48"	41''
Max Allowable Cantilever	Landscape	24"	NA
Standoff Configuration	Landscape	Staggered	
Max Standoff Tributary Area	Trib	14 sf	
PV Assembly Dead Load	W-PV	3.0 psf	
Net Wind Uplift at Standoff	T-actual	-153 lbs	
Uplift Capacity of Standoff	T-allow	548 lbs	
Standoff Demand/Capacity	DCR	28.0%	

		X-Direction	Y-Direction
Max Allowable Standoff Spacing	Portrait	48''	62"
Max Allowable Cantilever	Portrait	20''	NA
Standoff Configuration	Portrait	Staggered	
Max Standoff Tributary Area	Trib	21 sf	
PV Assembly Dead Load	W-PV	3.0 psf	
Net Wind Uplift at Standoff	T-actual	-232 lbs	
Uplift Capacity of Standoff	T-allow	548 lbs	
Standoff Demand/Capacity	DCR	42.3%	